

## FAILURE AND SURFACE TEMPERATURE ANALYSIS OF WORKING SURFACE OF DIE-CASTING DIE

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### ABSTRACT

*Die-casting is the most cost efficient and technical easy method of casting sophisticated and accurate aluminium alloys parts in great-scale series. Aluminium alloys die-castings require little machining prior the final installation.*

*Die-casting dies for casting of aluminium alloys fail because of a great number of different and simultaneously operating factors. Die design, material selection, and thermal stress fatigue generated by the cyclic working process, as well as to low and inhomogeneous initial die temperature contribute to the failures and cracks formation on/in dies for die-casting of aluminium alloys.*

*In the frame of the presented investigation work the intensity and homogeneity of the temperature, fields on the working surface of the testing die were checked through thermo graphic measurements, and failures and cracks on the working surface of the die were analysed with non-destructive metallographic examination methods.*

**Keywords:** die-casting die, failure analysis, working surface

### 1. INTRODUCTION

Aluminium die-casting dies fail because of a number of different and simultaneously operating stresses. The stresses are of two basic kinds [1] the first which are created during the manufacturing of the die, and the second which are produced during exploitation process.

For economical production of aluminium alloys die-castings it is important that the dies have a long working life. The replacement of a die is expensive in both: money and production time. The most frequent failures die-casting dies for aluminium alloys are [2]: heat checking, big cracks, cracking in corners, sharp radii, or sharp edges, and cracking due to wear or erosion.

It is generally agreed that one of the principal causes of termination of die life is heat checking, which occurs through a process of crack initiation and propagation from the thermal stress fatigue induced on a die surface [3,4]. Some of the factors that affect die failures may be controlled to some extent by the die-casting experts (designers, manufacturers and operators). These factors include [5]: design, materials selection, heat treatment, finishing operations, and handling and use.

## 2. DIES AND MATERIALS PROPERTIES

In the frame of our investigation work a complex analysis of a typical dies for die-casting of aluminium alloys has been carried out. The testing die-casting die is shown in Figure 1.



Figure 1. Fixed half of the die-casting die.

The die was made from the well known BOEHLER W300 ISODISC [6] hot work tool steel. This steel is mostly applied and considered material for all kinds of hot working dies. The chemical composition of the steel is given in the Table 1.

Thermal and mechanical properties of BOEHLER W300 ISODISC steel are well known. Liquidus temperature of casted aluminium alloy AlSi9Cu3 is approximately 593 °C, and casting temperature is approximately 50 °C higher, therefore the properties in the temperature interval from the ambient temperature up to approximately 700 °C are important for the analysis of the discussed case.

Table 1. Chemical composition of BOEHLER W300 ISODISC steel [6]

| Element   | C    | Si   | Mn   | Cr   | Mo   | V    |
|-----------|------|------|------|------|------|------|
| (mass. %) | 0.38 | 1.10 | 0.40 | 5.00 | 1.30 | 0.40 |

The density of BOEHLER W300 ISODISC steel at 20 °C is approximately 7800 kg/m<sup>3</sup>, and it decreases with higher temperature. Up to the temperature of 700 °C it drops for about 200 kg/m<sup>3</sup>. This steel has relatively low and nearly linear increasing heat conductivity (19.2 to 26.3 W/m·K), and proportionally constant thermal diffusivity (the whole time approximately 5·10<sup>-6</sup> m<sup>2</sup>/s). Specific heat is increased with higher temperature and it is from 456 to 587 J/kg·K, respectively, for the boundary values of the chosen temperature range. Linear coefficient of elongation slowly increases from 10.7·10<sup>-6</sup> /K (at 20 °C) to 13.2·10<sup>-6</sup> /K (at 700 °C), while the modulus of elasticity, with boundary values of 211 and 168 GPa, decreases with the increase of temperature.

## 3. TEMPERATURE FIELD ANALYSIS

When hot aluminium alloy melt wets the active working surface of the die, the die expands and then contracts during cooling, as the heat in the casting is conducted into the steel below the surface of the die. The greater difference between the temperature of the die and that of the hot aluminium shot into the die, the greater will be the expansion and contraction of the die surface, and sooner the die surface will be heat check. Since the stresses produced on the die surface are inversely proportional to the die temperature, it is good practice to run the dies as hot as is practical and/or economical. Aluminium die-casting dies should be preheated to approximately 240 to 300 °C. Experiences have shown that by increasing the die operating temperature from 205 to 315 °C, die production may be doubled.

By thermo graphic measurements the required intensity and homogeneity of the initial temperature field on the working surface of the fixed die half have been examined (Figure 2). Testing thermo graphic measurements on the chosen die have been carried out due to the relatively simple geometry of the discussed die (see Figure 1), so the simple thermographs (heat images) analysis has been performed. In comparison with optical pyrometers, which application is limited to the very small surface, investigated object is enabled by thermo graphic camera. Camera field vision is about 30 ° horizontally and 20 ° vertically. Within that field of vision the temperature image of about 30.000 information points or temperature patterns has been formed by the camera. The geometric resolving power of single details depends on the distance of camera to object.

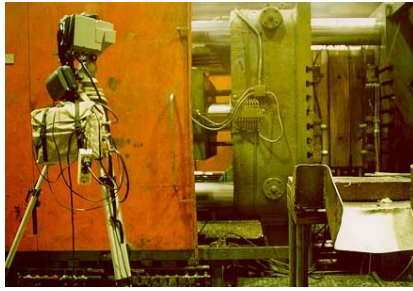


Figure 2. Position of the thermo graphic camera (FLIR ThermoCam PM675).

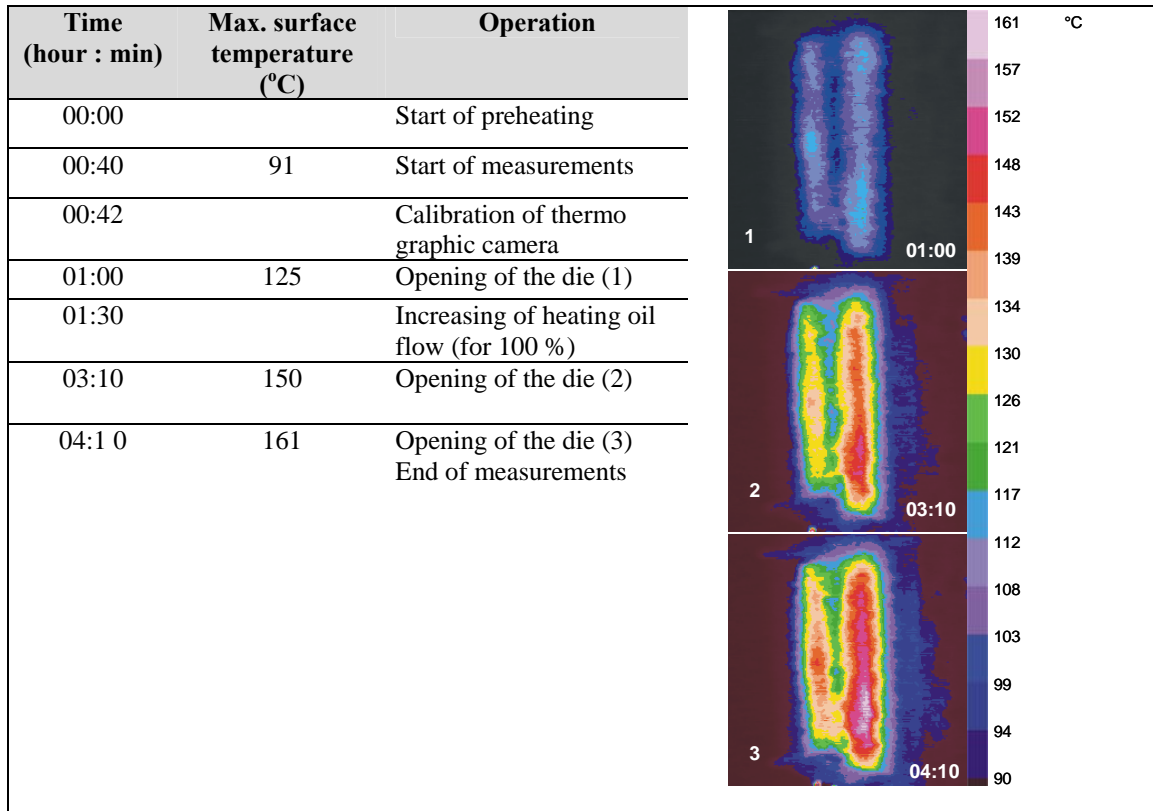


Figure 3. Working surface of the fixed part of the die-casting die. Testing case - chronological flow of the preheating process. Thermograph: at the beginning (1), after approx. 2 hours (2) and at the end (3 – initial temperature field) of the die preheating process.

On the working surface of the fixed half of the die thermo graphic measurements have been carried out in the preheating period of the die heating to its initial operating temperature. Checking temperature measurements on the die surface and calibration of the thermo graphic camera have been carried out using contact Ni-NiCr thermometer. By the contact thermometer the temperature of 61.2 °C was measured at time of 00:42 in the given and marked point on the surface of the fixed half of the die, a few seconds later the thermo graphic camera (calibrated for the virtual value of emissivity equal 1.0) has been directed to the same point with the virtual temperature of 67.1 °C. The ratio between both measured temperatures was the value of emissivity of 0.91, which was not automatically considered by non-directed thermo graphic camera. The emissivity has to be determined experimentally before each measurement. Thermographs, shown in Figure 3, are just parts of longer continuous prints. The temperature distribution on working surface of the die-casting die is evidently presented on coloured thermographs. Black and white thermographs have been coloured with sixteen sober colours. Sober transitions between colours more evidently illustrate differences between all temperatures, while the geometric details are less clear. For each thermograph the time of formation of image print is very important. The first thermograph is presented with extended colour scale to be directly comparable to the next two, which were done later, when the surface temperatures of the

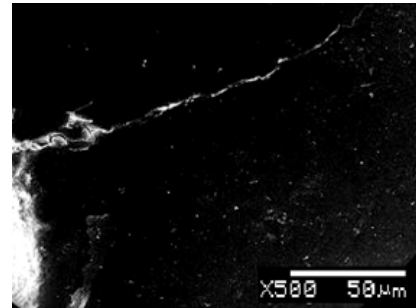
preheated die have been essentially higher. Only the same temperature range coloured thermographs should be directly compared. Thermographs are presented in the temperature range between 90 and 161 °C, where uncoloured (black) regions are below 90 °C.

In the foundry praxis preheating times of similar dies are much shorter than they should be during our testing (maximally up to two hours). Furthermore the flow of heating oil (with the temperature approximately 250 °C) was increased during our testing measurements after approximately one hour from 30 l/min (usually applied in the foundry praxis) to 60 l/min. Regarding to the presented parameters the practical results of preheating of the discussed die can be mostly worse comparing to the results of the testing thermograph measurements.

#### 4. FAILURE ANALYSIS

The cracks which appeared on the working surface of the fixed die half after less than thousand shots were revealed and identified by the use of penetrants. Some of them were also clearly seen by the use of magnifying glass or even by naked eye. In the frame of our experimental work also non-destructive metallographic examination by optical microscopy (OM) and by scanning electron microscopy (SEM) of polymeric replicas was applied.

*Figure 4. Working surface of the testing die-casting die. Surface crack (approx. 150 µm long) and pits. SEM.*



The failures observed on the working surface (Figure 4) belong to heat checking initiated at identification marks, and cracking in corners, sharp edges and transitions.

#### 5. CONCLUSIONS

Cracking on/in die-casting dies for aluminium alloys is caused by a number of different and simultaneously operating factors. Some of them, that affect die failures, may be controlled to some extent by the die-casting experts. Beside, the die design, the material selection and the process thermal stress fatigue course, which is the consequence of the working conditions, the inhomogeneous and to low initial temperature of the die, contribute to the cracks formation.

It is clearly seen from the presented thermographs, that the required temperatures and homogeneity of the temperature field of the discussed case are not possible to reach without the changing both: the heating method and the die design. In the process of the die-casting the primary source of loading is cyclic variation of the temperature; the influence of other loads is relatively insignificant. Therefore in the first stage a solution of the problem should be in changing of the position of heating and/or cooling channels, i.e. their closer shifting to the working surface of the die, so the higher and more homogeneous heating should be reached.

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